

## 5.4: Deposition of Iron

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- ❖ Need to study this reaction-Rusting of iron
- ❖ Conventional analysis-Overall reaction-“ $\text{Fe}^{2+} + 2\text{e} \rightarrow \text{Fe}$ ” Two faradays current for every one mole of iron deposited from  $\text{Fe}^{2+}$ .
- ❖ One can look for the transfer coefficients and electrochemical reaction orders.
- ❖ The **anodic Tafel slope** of the plot of “ $\Delta\Phi$  vs  $\log i$ ” OR “ $(\eta$  vs  $\log i)$ ” was found to be **0.04**

$$\frac{d \Delta\Phi}{d \log i} = \frac{2.303RT}{\alpha F} = 0.04 ; \quad \alpha = 1\frac{1}{2}$$

**Note:**

$$i = i_0 e^{\alpha \eta F / RT} \text{ (Anodic process)}$$

$$\ln i = \frac{\alpha \eta F}{RT} + \ln i_0$$

$$\eta = \frac{2.303RT}{\alpha F} \log i - \frac{2.303RT}{\alpha F} \log i_0$$

- ❖ Similarly the magnitude of the **cathodic Tafel slope** of the plot of  $\Delta\Phi$  vs  $\log i$  ( $\eta$  vs  $\log i$ ) was found to be **0.12**

$$\frac{d \Delta\Phi}{d \log i} = \frac{2.303RT}{\beta F} = 0.12 ; \quad \beta = \frac{1}{2}$$

$$v = \frac{n}{\alpha + \beta} = \frac{2}{1\frac{1}{2} + \frac{1}{2}} = 1$$

**NOTE:** The conventional plot should be  $\log i$  vs  $\eta$ . In which case the expression for slope would be the reciprocal of what are mentioned above.

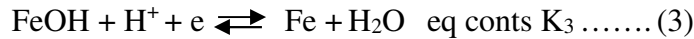
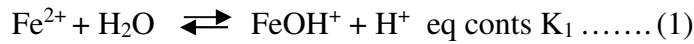
- ❖ Therefore, the rds occurs once per the occurrence of the overall reaction since,  $v=1$ .
- ❖ The discharge reaction was found to be is **1<sup>st</sup> order** with respect to  $\text{Fe}^{2+}$  and  $\text{OH}^-$ .
- ❖ Thus the mechanism proposed for iron dissolution reaction must account for the following :

$$\alpha = 1\frac{1}{2}, \quad \beta = \frac{1}{2}, \quad v = 1, \text{ The reaction order: } \rho_{\text{OH}^-} = 1 \text{ (on both direction) and}$$

5.4: Deposition of Iron

$$\rho_{\text{Fe}^{2+}} = 1$$

❖ Consider the following mechanism.



**Step-1:** Fast chemical equilibrium

Law mass action & Equilibrium constant

**Step-2:** Slow electrochemical equilibrium-RDS (**Actual rds**)

Anodic & cathodic currents are not equal; Nett current is not equal zero

**Step-3:** Fast electrochemical equilibrium

Anodic & cathodic currents are equal

The equation for the multistep step reaction is

$$i = i_0 [e^{\alpha_F \eta / RT} - e^{-\beta_F \eta / RT}]$$

**NOTE:-**

- *Equilibrium step (RDS) nett c.d is not zero, if it is electrochemical*
- *Equilibrium step (Not RDS) nett c.d is zero, if it is electrochemical*

**I. Assume STEP-3 as RDS.**

Rate = Rate of rds = Magnitude of net c.d. of rds ,

$$i_{\text{rds}} = i_a - i_c$$

$$i = 1.F [k_{-3}(1 - \theta_{\text{FeOH}})e^{(1-\beta)\Delta\Phi_F / RT} - k_3 \theta_{\text{FeOH}} [\text{H}^+]e^{-\beta\Delta\Phi_F / RT}] \dots\dots\dots (4)$$

$$= 1.F [k_{-3}e^{(1-\beta)\Delta\Phi_F / RT} - k_3 \theta_{\text{FeOH}} [\text{H}^+]e^{-\beta\Delta\Phi_F / RT}]; \text{for } \theta_{\text{FeOH}} \ll 1 \dots\dots\dots (4a)$$

**Step-3 assumed to be RDS. Hence net current is not equal**

*The intermediate FeOH could be considered as a precipitate .Hence,the surface of Fe will be covered with a coating of FeOH. Therefore, the activity of Fe will not be one.But (1-θ<sub>FeOH</sub>) and the activity (concentration) of FeOH will be θ<sub>FeOH</sub>.*

**Note:** θ<sub>FeOH</sub> in equation-4(a) must be eliminated.

The 2<sup>nd</sup> step is a fast electroequilibrium electrochemical process v<sub>-2</sub> = v<sub>2</sub> or i<sub>-2</sub> = i<sub>2</sub>

**5.4: Deposition of Iron**

$$k_{-2} \theta_{\text{FeOH}} e^{(1-\beta)\Delta F/RT} = k_2 [\text{FeOH}^+] e^{-\beta\Delta\Phi F/RT} \dots\dots\dots (5)$$

The species FeOH<sup>+</sup> will be in solution

$$\theta_{\text{FeOH}} = K_2 [\text{FeOH}^+] e^{-\beta\Delta\Phi F/RT} \dots\dots\dots (6)$$

The concentration of FeOH<sup>+</sup> can be determined from the chemical **step-1**. (Eq-1) as follows:

$$[\text{FeOH}^+] [\text{H}^+] [\text{Fe}^{2+}]^{-1} = K_1$$

Therefore,  $[\text{FeOH}^+] = K_1 [\text{H}^+]^{-1} [\text{Fe}^{2+}] \dots\dots\dots (7)$

Hence, substitute  $[\text{FeOH}^+] = K_1 [\text{H}^+]^{-1} [\text{Fe}^{2+}]$  in equation-(6)

$$\theta_{\text{FeOH}} = K_1 K_2 [\text{Fe}^{2+}] [\text{H}^+]^{-1} e^{-\Delta\Phi F/RT} \dots\dots\dots (8)$$

Substituting for  $[\text{FeOH}^+]$  &  $\theta_{\text{FeOH}}$  in equation-4a

$$i = F \{ k_{-3} e^{(1-\beta)\Delta\Phi F/RT} - k_3 K_1 K_2 [\text{Fe}^{2+}] e^{-\Delta\Phi F/RT} e^{-\beta\Delta\Phi F/RT} \} \dots\dots\dots (9)$$

The dissolution reaction (cathodic reaction) order looks to be zero w.r.t. H<sup>+</sup> & OH<sup>-</sup> and 1 w.r.t Fe<sup>2+</sup>.

**But , it has been found to be first – order w.r.t H<sup>+</sup> .**

Moreover, the final equation could be written as

$$i = i_0 [e^{(1-\beta)\eta F/RT} - e^{-(1+\beta)\eta/RT}]$$

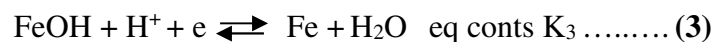
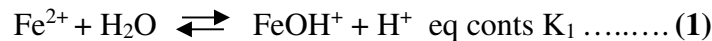
Hence,  $\alpha \leftarrow = 1/2$  and  $\alpha \rightarrow = 1/2$

But, the values have been found to be

$$\alpha \leftarrow = 1/2 \text{ and } \alpha \rightarrow = 1/2$$

**“Therefore STEP-3 is not rds !!!!”.**

**II. Assume Step - 2 as RDS.**



The B.V. eq for the rds (step-2) is

$$i = F k_{-2} \theta_{\text{FeOH}} e^{(1-\beta)\Delta\Phi F/RT} - k_2 [\text{FeOH}^+] e^{-\beta\Delta\Phi F/RT} \text{ for } \theta_{\text{FeOH}} \ll 1 \dots\dots(4)$$

5.4: Deposition of Iron

*Step-2(slow electrochemical equilibrium) is assumed to be RDS. Hence net current is not equal*

**NOTE :** The terms ,  $\theta_{\text{FeOH}}$  &  $[\text{FeOH}^+]$  in equation-4 must be eliminated

From the electrochemical equilibrium **step- 3.**  $v_a = v_c$

$$\text{i.e., } F k_{-3}(1-\theta_{\text{FeOH}}) e^{(1-\beta)\Delta\phi F/ RT} = Fk_3\theta_{\text{FeOH}}[\text{H}^+]e^{-\beta\Delta\phi F/ RT}$$

$$F k_{-3}e^{(1-\beta)\Delta\phi F/ RT} = Fk_3\theta_{\text{FeOH}}[\text{H}^+]e^{-\beta\Delta\phi F/ RT} \quad ; \text{ for } \theta_{\text{FeOH}} \ll 1$$

$$\theta_{\text{FeOH}} = \frac{1}{K_3} [\text{H}^+]^{-1} e^{\Delta\phi F/ RT}$$

$$[\text{H}^+][\text{OH}^-] = K_w = 1 \times 10^{-14}$$

$$[\text{H}^+]^{-1} = \frac{[\text{OH}^-]}{K_w}$$

$$\theta_{\text{FeOH}} = \frac{1}{K_3 K_w} [\text{OH}^-]e^{\Delta\phi F/ RT} \dots\dots\dots(5)$$

The expression for  $[\text{FeOH}^+]$  can be obtained as follows:

From **step-1(Fast chemical equilibrium),**

$$[\text{FeOH}^+] = \frac{K_1 [\text{Fe}^{2+}][\text{H}^+]}{[\text{Fe}^{2+}]} ; \text{ (Law of mass action) } \dots\dots\dots(6)$$

But,  $[\text{H}^+] = \frac{[\text{OH}^-]}{K_w}$

Therefore,  $[\text{FeOH}^+] = \frac{K_1 [\text{Fe}^{2+}][\text{OH}^-]}{K_w} \dots\dots\dots(7)$

Substituting for  $\theta_{\text{FeOH}}$  and  $[\text{FeOH}^+]$  , from equations-5 & 7 , in Eq-4 , the

5.4: Deposition of Iron

B.V. eq for rds becomes

$$i = k[\text{OH}^-]e^{(2-\beta)\Delta\phi F/RT} - k'[\text{Fe}^{2+}][\text{OH}^-] e^{-\beta\Delta\phi F/RT} \dots\dots\dots(8)$$

Therefore, the anodic order is 1 w.r.t : OH<sup>-</sup> ; cathodic order is 1 w.r.t both Fe<sup>2+</sup> and OH<sup>-</sup>

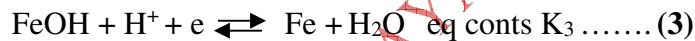
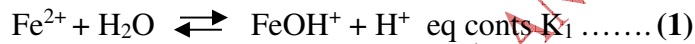
Replacing ΔΦ by ΔΦ<sub>e</sub> + η, and thereby factorizing the exchange current density, i<sub>0</sub> we get

$$i = i_0[e^{(2-\beta)\eta F/RT} - e^{-\beta\eta F/RT}] \dots\dots\dots(9)$$

Hence, the anodic and cathodic transfer coefficients are α<sup>←</sup> = 1/2 and α<sup>→</sup> = 1/2

Therefore, the mechanism with “Step-2 as rds” is the correct one

The transfer coefficients can be evaluated theoretically.



Note:

$$\alpha^{\leftarrow} = (\gamma^{\leftarrow}/v) + r - r\beta \quad \& \quad \alpha^{\rightarrow} = (\gamma^{\rightarrow}/v) + r\beta$$

γ<sup>→</sup>: No. of electrochemical step(s) before rds

γ<sup>←</sup>: No. of electrochemical step(s) after rds

Step-3 rds : Not ok

$$\gamma^{\leftarrow} = 0 \ ; \ \gamma^{\rightarrow} = 1 \ ; \ v = 1 \ ; \ r = 1 \ ; \ \alpha^{\leftarrow} = 1/2 \ \& \ \alpha^{\rightarrow} = 1$$

Step-2 rds : OK

$$\gamma^{\leftarrow} = 1 \ ; \ \gamma^{\rightarrow} = 0 \ ; \ v = 1 \ ; \ r = 1 \ ; \ \alpha^{\leftarrow} = 3/2 \ \& \ \alpha^{\rightarrow} = 1/2$$

Step-1 rds: Not ok

$$\gamma^{\leftarrow} = 2 \ ; \ \gamma^{\rightarrow} = 0 \ ; \ v = 1 \ ; \ r = 0 \ ; \ \alpha^{\leftarrow} = 2 \ \& \ \alpha^{\rightarrow} = 0$$

HW: Calculate the theoretical Anodic & Cathodic Tafel slope of “lni vs η” in each case